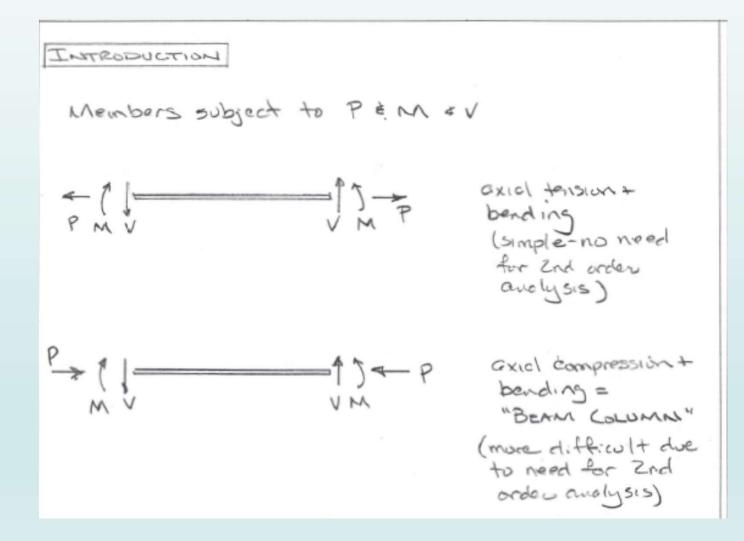
# **Design of Beam-Columns**

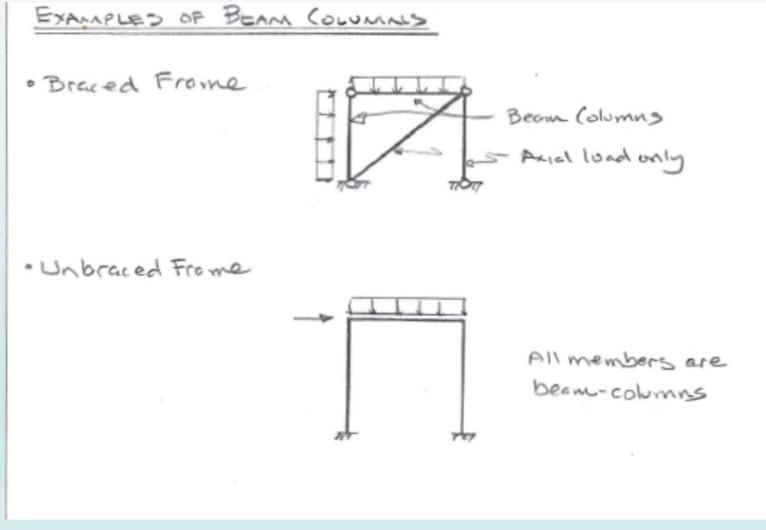
## **Beam-Column - Outline**

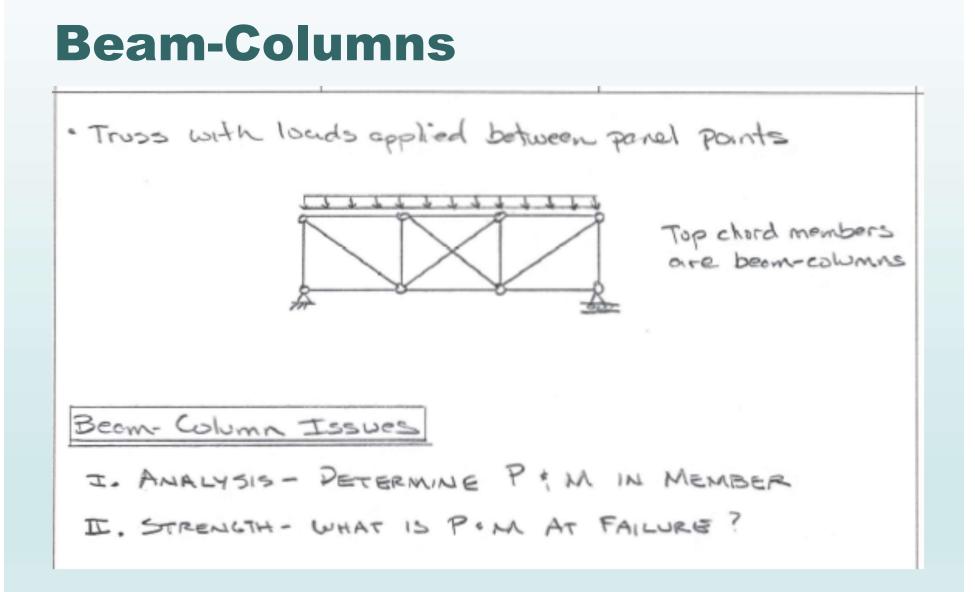
- Beam-Columns
- Moment Amplification Analysis
- Second Order Analysis
- Compact Sections for Beam-Columns
- Braced and Unbraced Frames
- Analysis/Design of Braced Frames
- Analysis/Design of Unbraced Frames
- Design of Bracing Elements

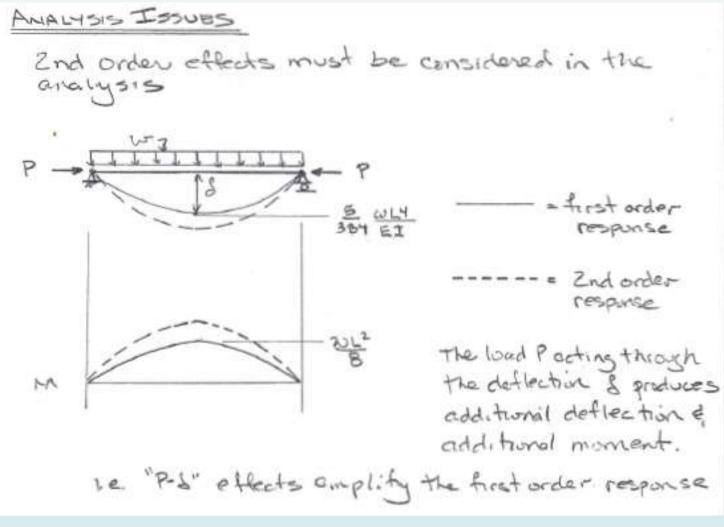
# **Design for Flexure – LRFD Spec.**

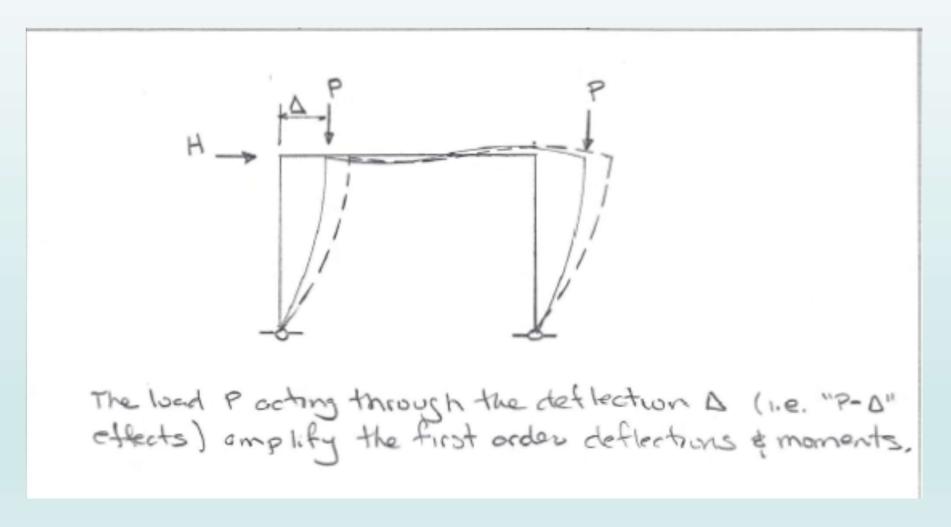
- Commonly Used Sections:
  - I shaped members (singly- and doubly-symmetric)
  - Square and Rectangular or round HSS

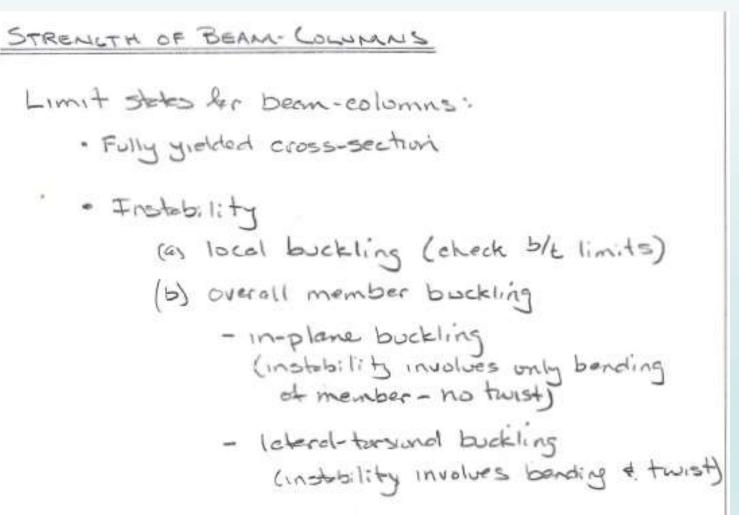












Likely failure modes due to combined bending and axial forces:

- Bending and Tension: usually fail by yielding
- Bending (uniaxial) and compression: Failure by buckling in the plane of bending, without torsion
- Bending (strong axis) and compression: Failure by LTB
- Bending (biaxial) and compression (torsionally stiff section): Failure by buckling in one of the principal directions.
- Bending (biaxial) and compression (thin-walled section): failure by combined twisting and bending
- Bending (biaxial) + torsion + compression: failure by combined twisting and bending

- Structural elements subjected to combined flexural moments and axial loads are called *beam-columns*
- **The case of beam-columns usually appears in structural frames**
- The code requires that the sum of the load effects be smaller than the resistance of the elements

$$\frac{\sum \gamma_i Q_i}{\phi R_n} \le 1.0$$

□ Thus: a column beam interaction can be written as

$$\frac{P_u}{\phi_c P_n} + \left[\frac{M_{ux}}{\phi_b M_{nx}} + \frac{M_{uy}}{\phi_b M_{ny}}\right] \le 1.0$$

□ This means that a column subjected to axial load and moment will be able to carry less axial load than if no moment would exist.

□ AISC code makes a distinct difference between lightly and heavily axial loaded columns

$$for \frac{P_u}{\phi_c P_n} \ge 0.2 \qquad \frac{P_u}{\phi_c P_n} + \frac{8}{9} \left[ \frac{M_{ux}}{\phi_b M_{nx}} + \frac{M_{uy}}{\phi_b M_{ny}} \right] \le 1.0$$

AISC Equation

for 
$$\frac{P_u}{\phi_c P_n} \le 0.2$$
  $\frac{P_u}{2\phi_c P_n} + \left[\frac{M_{ux}}{\phi_b M_{nx}} + \frac{M_{uy}}{\phi_b M_{ny}}\right] \le 1.0$ 

AISC Equation

#### Definitions

- $P_u$  = factored axial compression load
- $P_n$  = nominal compressive strength

 $M_{ux}$  = factored bending moment in the x-axis, including second-order effects

 $M_{nx}$  = nominal moment strength in the x-axis

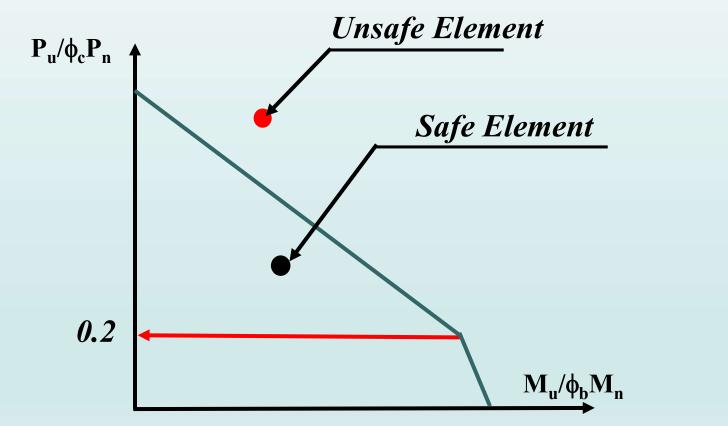
 $M_{uv}$  = same as  $M_{ux}$  except for the y-axis

 $M_{ny}$  = same as  $M_{nx}$  except for the y-axis

 $\phi_c$  = Strength reduction factor for compression members = 0.90

 $\phi_{\rm b}$  = Strength reduction factor for flexural members = 0.90

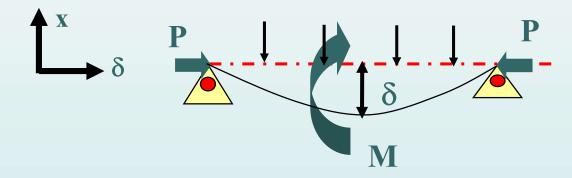
□ The increase in slope for lightly axial-loaded columns represents the less effect of axial load compared to the heavily axial-loaded columns



These are design charts that are a bit conservative than behaviour envelopes

# **Moment Amplification**

□ When a large axial load exists, the axial load produces moments due to any element deformation.



- □ The final moment "M" is the sum of the original moment and the moment due to the axial load. The moment is therefore said to be amplified.
- □ As the moment depends on the load and the original moment, the problem is nonlinear and thus it is called second-order problem.