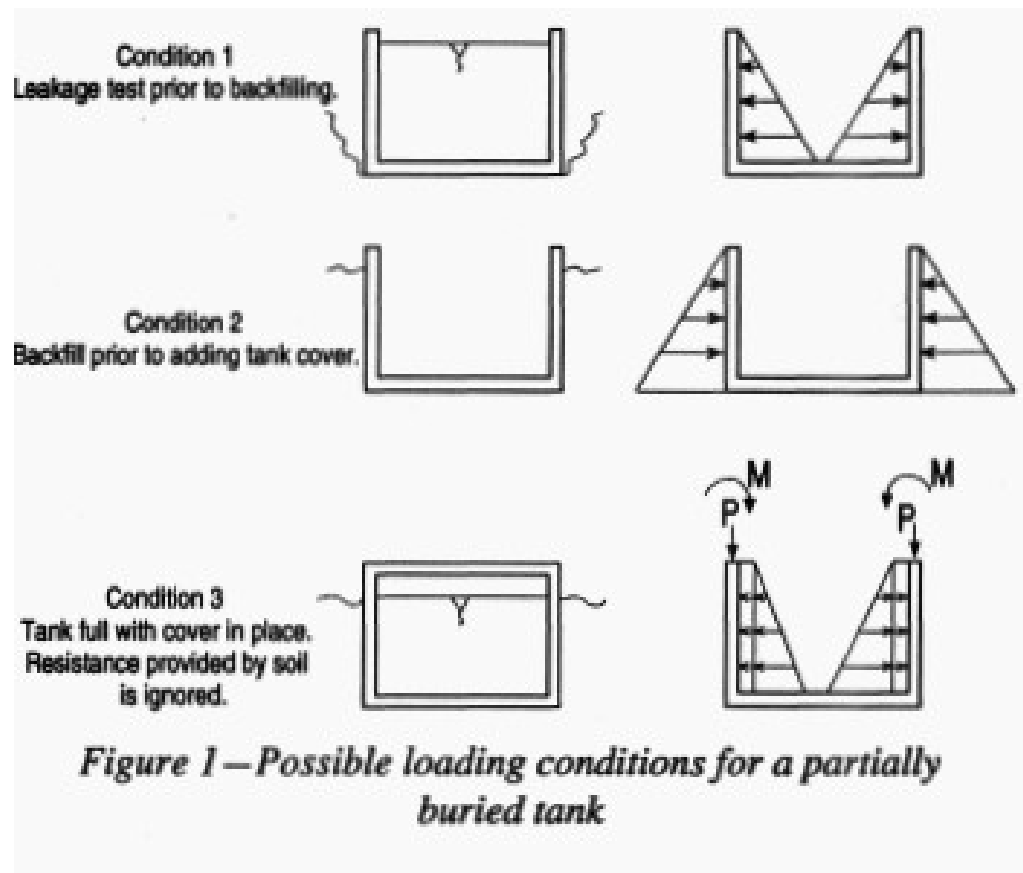

Design of Circular Concrete Tanks

Design of Circular Concrete Tanks

Load Conditions



Loading Conditions

- ✓ The tank may also be subjected to uplift forces from hydrostatic pressure at the bottom when empty.
- ✓ It is important to consider all possible loading conditions on the structure.
- ✓ Full effects of the soil loads and water pressure must be designed for without using them to minimize the effects of each other.
- ✓ The effects of water table must be considered for the design loading conditions.

Design of Circular Concrete Tanks

Strength Design Method

- **Modification 1** The load factor to be used for lateral liquid pressure, F , is taken as 1.7 rather than the value of 1.4 specified in ACI 318.
- **Modification 2** ACI 350-01 requires that the value of U be increased by using a multiplier called the sanitary coefficient.
Required strength = Sanitary coefficient \times U
where the sanitary coefficient equals:
 - 1.3 for flexure
 - 1.65 for direct tension
 - 1.3 for shear beyond that of the capacity provided by the Concrete.

Design of Circular Concrete Tanks

Working Stress Design

- ACI 350-01 implies in its document that the maximum allowable stress for Grade 60 (420 mpa) reinforcing steel is 210 mpa($0.5f_y$).
- ACI 350 recommends the allowable stress in hoop tension for Grade 60 (420 mpa) reinforcing steel as is 140 mpa($f_y/3$).

Modification according to ACI 350-06

Load Combinations according to ACI318-14

$$U = 1.4(D + F)$$

$$U = 1.2(D + F + T) + 1.6(L + H) + 0.5(Lr \text{ or } S \text{ or } R)$$

$$U = 1.2D + 1.6(Lr \text{ or } S \text{ or } R) + (1.0L \text{ or } 0.8W)$$

$$U = 1.2D + 1.6W + 1.0L + 0.5(Lr \text{ or } S \text{ or } R)$$

$$U = 1.2D + 1.2F + 1.0E + 1.6H + 1.0L + 0.2S$$

$$U = 0.9D + 1.2F + 1.6W + 1.6H$$

$$U = 0.9D + 1.2F + 1.0E + 1.6H$$

Modification according to ACI 350-06

Load Combinations:

L = live loads, or related internal moments and force

L_r = roof live load, or related internal moments and forces

D = dead loads, or related internal moments and forces

E = load effects of earthquake, or related internal forces

R = rain load, or related internal moments and forces

S = snow load, or related internal moments and forces

H = loads due to weight and pressure of soil, water in soil, or other materials, or related internal moments and forces

F = loads due to weight and pressures of fluids with well-defined densities and controllable maximum heights, or related internal moments and forces

Modification according to ACI 350-06

Durability Factor

Required strength environmental durability factor (S_d).

$$S_d = \frac{\phi f_y}{\gamma f_s} \geq 1.0$$

where : $\gamma = \frac{\text{factored load}}{\text{unfactored load}}$

$$\text{Required Strength} = S_d \cdot \text{factored load} = S_d \cdot U$$

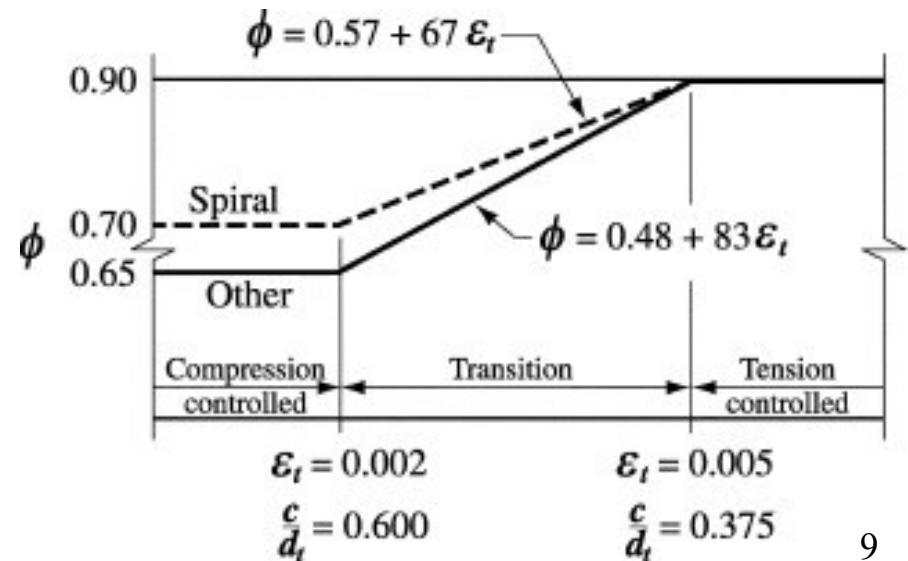
f_s is the permissible tensile stress in reinforcement

Design of Circular Concrete Tanks

Modification according to ACI 350-06

➤ **Strength reduction factor ϕ shall be as follows:**

- ✓ Tension-controlled sections $\phi=0.90$
- ✓ Compression-controlled sections,
 - ❖ Members with spiral reinforcement $\phi=0.70$
 - ❖ Other reinforced members $\phi=0.65$
- ✓ Shear and torsion $\phi=0.75$
- ✓ Bearing on concrete $\phi=0.65$



Modification according to ACI 350-06

Permissible Stresses

➤ Direct and hoop tensile stresses

Normal environmental exposures

$$f_s = 20 \text{ ksi (138 Mpa} \cong 140\text{Mpa)}$$

Severe environmental exposures

$$f_s = 17 \text{ ksi (117 Mpa} \cong 120\text{Mpa)}$$

➤ Shear stress carried by shear reinforcement

Normal environmental exposures

$$f_s = 24 \text{ ksi (165 Mpa)}$$

Severe environmental exposures

$$f_s = 20 \text{ ksi (138 Mpa} \cong 140\text{Mpa)}$$

Modification according to ACI 350-06

Shear Stress

Shear stress carried by the shear reinforcing is defined as the excess shear strength required in addition to the design shear strength provided by the concrete ϕV_c

$$\phi V_s \geq S_d (V_u - \phi V_c)$$

Modification according to ACI 350-06

Permissible Stresses

➤ Flexural stress

Normal environmental exposures

$$f_{s,\max} = \frac{320}{\beta \sqrt{s^2 + 4(2 + d_b/2)^2}} \geq 20\text{ksi} (\cong 140\text{Mpa}) \text{ for one way members}$$
$$\geq 24\text{ksi} (165\text{Mpa}) \text{ for two way members.}$$

The following simplified equation can be used

$$f_{s,\max} = \frac{320}{\beta \sqrt{s^2 + 25}}$$

where: $\beta = \frac{h-c}{d-c}$

$\beta = 1.2$ for $h \geq 16$ in (40cm).

$\beta = 1.35$ for $h < 16$ in (40cm).

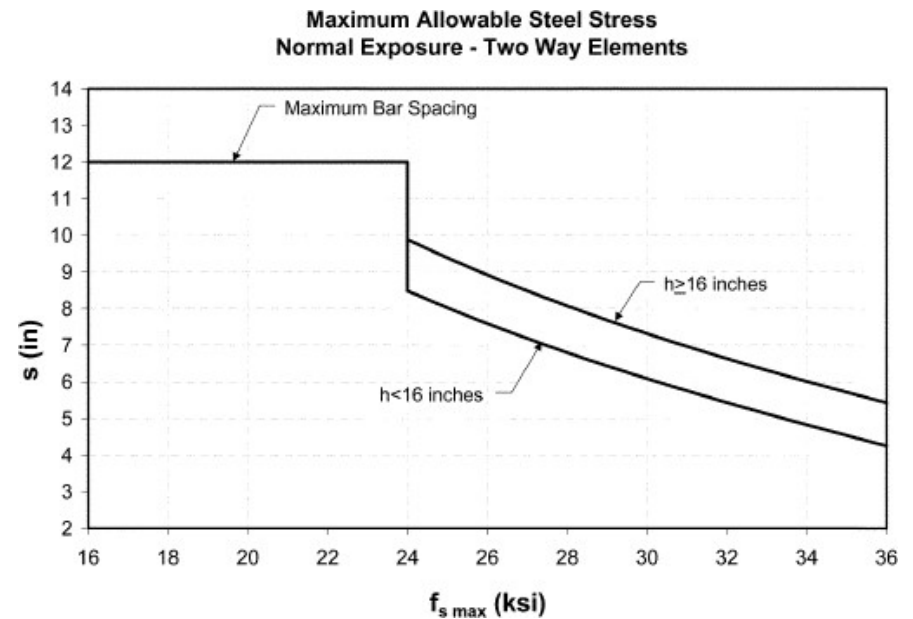
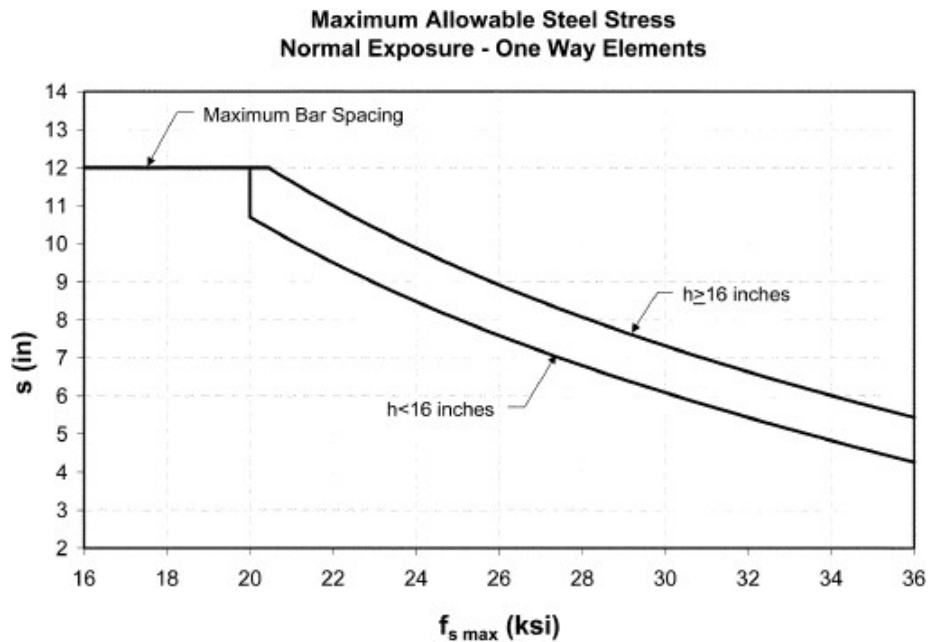
s = center-to-center spacing of deformed bars

Modification according to ACI 350-06

Permissible Stresses

➤ Flexural stress

Normal environmental exposures



Modification according to ACI 350-06

Permissible Stresses

➤ Flexural stress

Severe environmental exposures

$$f_{s,\max} = \frac{260}{\beta \sqrt{s^2 + 4(2 + d_b/2)^2}} \geq 17\text{ksi} (\cong 120\text{Mpa}) \text{ for one way members}$$
$$\geq 20\text{ksi} (\cong 140\text{Mpa}) \text{ for two way members.}$$

The following simplified equation can be used

$$f_{s,\max} = \frac{260}{\beta \sqrt{s^2 + 25}}$$

s = center-to-center spacing of deformed bars

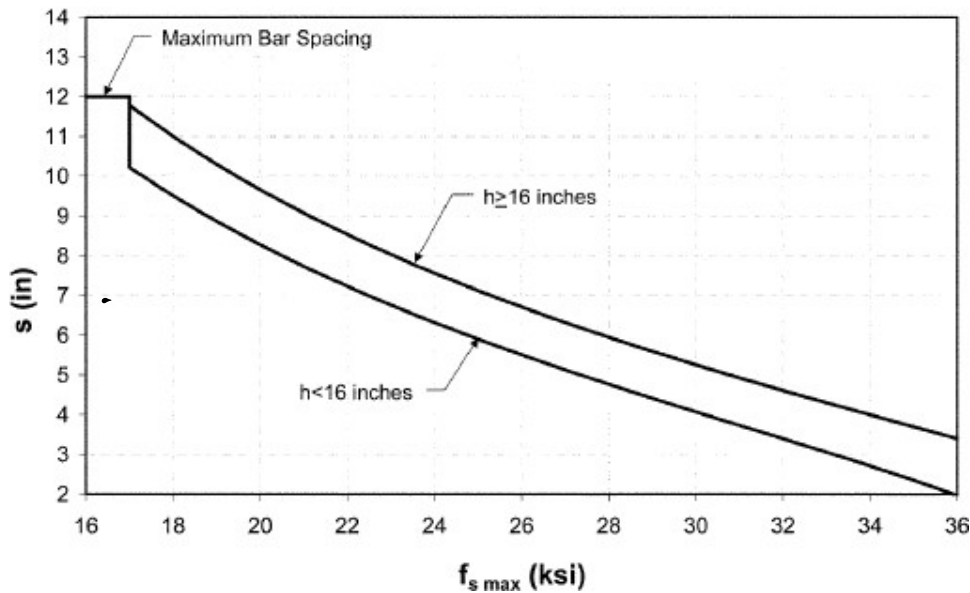
Modification according to ACI 350-06

Permissible Stresses

➤ Flexural stress

Severe environmental exposures

Maximum Allowable Steel Stress
Severe Exposure - One Way Elements



Maximum Allowable Steel Stress
Severe Exposure - Two Way Elements

