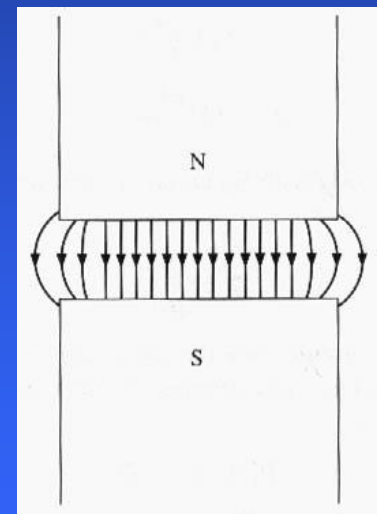


# 3. The magnetic field

Calculations of magnetic flux are **always** approximations!

1. We assume that all flux is confined within the magnetic core but a leakage flux exists outside the core since permeability of air is non-zero!
2. A mean path length and cross-sectional area are assumed...
3. In ferromagnetic materials, the permeability varies with the flux.
4. In air gaps, the cross-sectional area is bigger due to the fringing effect.

$$F = \phi R$$

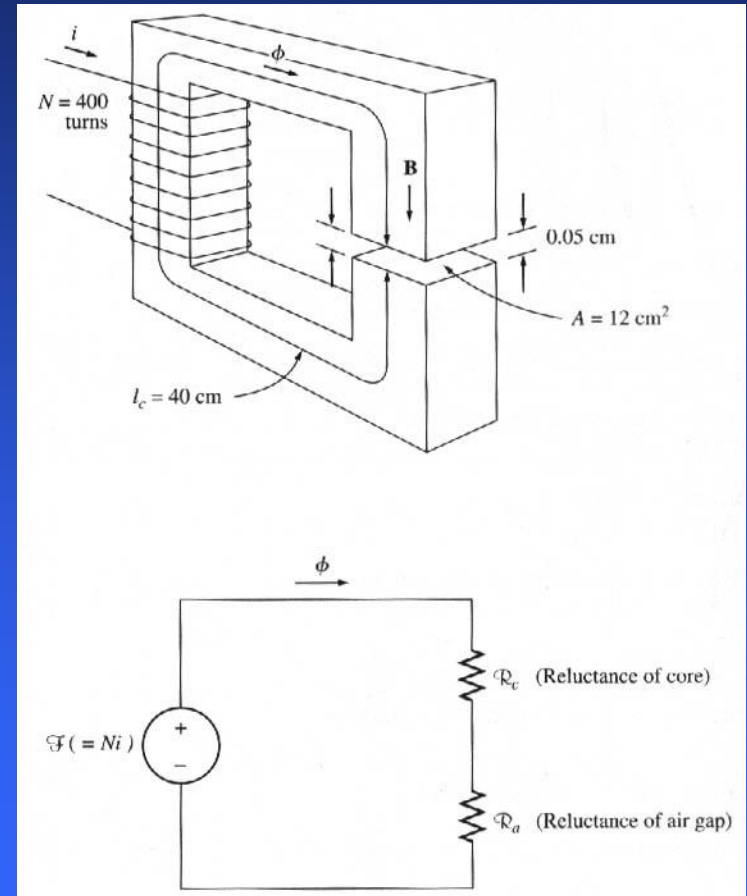


# 3. The magnetic field

Example 1: A ferromagnetic core with a mean path length of 40 cm, an air gap of 0.05 cm, a cross-section 12 cm<sup>2</sup>, and  $\mu_r=4000$  has a coil of wire with 400 turns. Assume that fringing in the air gap increases the cross-sectional area of the gap by 5%, find (a) the total reluctance of the system (core and gap), (b) the current required to produce a flux density of 0.5 T in the gap.

$$F = \phi R$$

The equivalent circuit



# 3. The magnetic field

(a) The reluctance of the core:

$$\mathcal{R}_c = \frac{l_c}{\mu A_c} = \frac{l_c}{\mu_0 \mu_r A_c} = \frac{0.4}{4000 \cdot 4\pi \cdot 10^{-7} \cdot 0.0012} = 66\,300 \text{ A-turns / Wb}$$

Since the effective area of the air gap is  $1.05 \times 12 = 12.6 \text{ cm}^2$ , its reluctance:

$$\mathcal{R}_a = \frac{l_a}{\mu_0 A_a} = \frac{0.0005}{4\pi \cdot 10^{-7} \cdot 0.00126} = 316\,000 \text{ A-turns / Wb}$$

The total reluctance:

$$\mathcal{R}_{eq} = \mathcal{R}_c + \mathcal{R}_a = 66\,300 + 316\,000 = 382\,300 \text{ A-turns / Wb}$$

The air gap contribute most of the reluctance!

# 3. The magnetic field

(b) The mmf:

$$F = \phi \mathcal{R} = Ni = B A \mathcal{R}$$

Therefore:

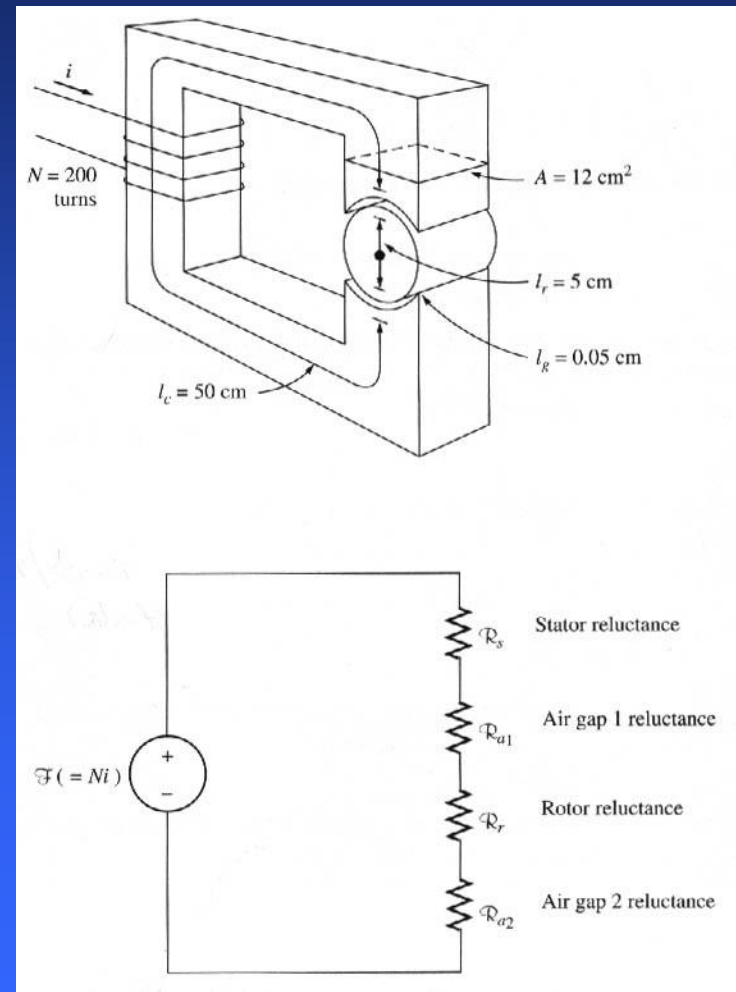
$$i = \frac{B A \mathcal{R}}{N} = \frac{0.5 \cdot 0.00126 \cdot 383200}{400} = 0.602 \text{ A}$$

Since the air gap flux was required, the effective area of the gap was used.

# 3. The magnetic field

Example 2: In a simplified rotor and stator motor, the mean path length of the stator is 50 cm, its cross-sectional area is  $12 \text{ cm}^2$ , and  $\mu_r = 2000$ . The mean path length of the rotor is 5 cm and its cross-sectional area is also  $12 \text{ cm}^2$ , and  $\mu_r = 2000$ . Each air gap is 0.05 cm wide, and the cross-section of each gap (including fringing) is  $14 \text{ cm}^2$ . The coil has 200 turns of wire. If the current in the wire is 1A, what will the resulting flux density in the air gaps be?

The equivalent circuit



# 3. The magnetic field

The reluctance of the stator is:

$$\mathcal{R}_s = \frac{l_s}{\mu_r \mu_0 A_s} = \frac{0.5}{2000 \cdot 4\pi \cdot 10^{-7} \cdot 0.0012} = 166000 \text{ A-turns/Wb}$$

The reluctance of the rotor is:

$$\mathcal{R}_r = \frac{l_r}{\mu_r \mu_0 A_r} = \frac{0.05}{2000 \cdot 4\pi \cdot 10^{-7} \cdot 0.0012} = 16600 \text{ A-turns/Wb}$$

The reluctance of each gap is:

$$\mathcal{R}_a = \frac{l_a}{\mu_0 A_a} = \frac{0.0005}{4\pi \cdot 10^{-7} \cdot 0.0014} = 284000 \text{ A-turns/Wb}$$

The total reluctance is:

$$\mathcal{R}_{eq} = \mathcal{R}_s + \mathcal{R}_{a1} + \mathcal{R}_r + \mathcal{R}_{a2} = 751000 \text{ A-turns/Wb}$$

# 3. The magnetic field

The net mmf is:

$$F = Ni$$

The magnetic flux in the core is:

$$\phi = \frac{F}{\mathcal{R}} = \frac{Ni}{\mathcal{R}}$$

Finally, the magnetic flux density in the gap is:

$$B = \frac{\phi}{A} = \frac{Ni}{\mathcal{R}A} = \frac{200 \cdot 1}{751000 \cdot 0.0014} = 0.19 \text{ T}$$