2. Getting DC voltage out of a rotating loop

A voltage out of the loop is alternatively a constant positive value and a constant negative value.

One possible way to convert an alternating voltage to a constant voltage is by adding a

commutator segment/brush circuitry to the end of the loop. Every time the voltage of the loop switches direction, contacts switch connection.

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The tangential velocity of the loop's edges is

$$
v = r\omega \tag{5.8.1}
$$

where r is the radius from the axis of rotation to the edge of the loop. The total induced voltage:

2 0 *tot* edge of the loop. The total induced **v**
 $e_{\text{tot}} = \begin{cases} 2 \text{r} \omega B l & \text{under the pole faces} \end{cases}$ *beyond the pole edges* of the loop. The total induced vo
 $\int 2 r \omega B l$ under the pole faces $=\left\{ \right.$ $\begin{cases} 2r\omega Bl & \text{under the pole faces} \\ 0 & \text{beyond the pole edges} \end{cases}$ (5.8.2)

The rotor is a cylinder with surface area $2\pi r l$. Since there are two poles, the area of the rotor under each pole is $A_p = \pi r l$. Therefore:

 ω

$$
e_{\rm tot} = \begin{cases} \frac{2}{\pi} A_p B \\ 0 \end{cases}
$$

S $A_p = \pi n$. **Therefore**.
 $\begin{cases} 2 \\ -R_p B\omega \end{cases}$ under the pole faces $\begin{cases} -A_p b\omega & \text{under the pole places} \\ 0 & \text{beyond the pole edges} \end{cases}$

(5.8.3)

Assuming that the flux density B is constant everywhere in the air gap under the pole faces, the total flux under each pole is

$$
\phi = A_p B \tag{5.9.1}
$$

(5.9.2)

The total voltage is

$$
e_{\text{tot}} = \begin{cases} \frac{2}{\pi} \phi \omega & \text{under the pole faces} \\ 0 & \text{beyond the pole edges} \end{cases}
$$

The voltage generated in any real machine depends on the following factors:

- 1. The flux inside the machine;
- 2. The rotation speed of the machine;
- 3. A constant representing the construction of the machine.

3. The induced torque in the rotating loop

Assuming that a battery is connected to the DC machine, the force on a segment of a loop is:

> $\overline{F} = i(\overline{\mathbf{I}} \times \mathbf{B})$ (12.1)

And the torque on the segment is

$$
\tau = rF \sin \theta \tag{5.12.2}
$$

Where θ is the angle between r and F. Therefore, the torque is zero when the loop is beyond the pole edges.

When the loop is under the pole faces:

1. Segment ab: $F_{ab} = i(\mathbf{1} \times \mathbf{B}) = i\mathbf{B}$ (5.13.1)

$$
F_{ab} = i(\mathbf{1} \times \mathbf{B}) = ilB
$$
\n
$$
\tau_{ab} = rF \sin \theta = r(iB) \sin 90^\circ = rilB \quad ccw
$$
\n(5.13.1)\n(5.13.2)

2. Segment bc: $F_{ab} = i(1 \times B) = 0$ (5.13.3)

$$
\tau_{ab} = rF \sin \theta = 0 \tag{5.13.4}
$$

3. Segment cd: $F_{ab} = i(\mathbf{1} \times \mathbf{B}) = i\mathbf{B}$ $F_{ab} = i(\mathbf{1} \times \mathbf{B}) = i\mathbf{B}$
 $\tau_{ab} = rF \sin \theta = r(i\mathbf{B}) \sin 90^\circ = ri\mathbf{B}$ *ccw* (5.13.5)

$$
\tau_{ab} = rF \sin \theta = r \left(ilB \right) \sin 90^\circ = rilB \quad ccw \tag{5.13.6}
$$

4. Segment da: $F_{ab} = i(1 \times B) = 0$ $\tau_{ab} = rF\sin\theta = 0$ (5.13.7) (5.13.8)

The resulting total induced torque is

$$
\tau_{ind} = \tau_{ab} + \tau_{bc} + \tau_{cd} + \tau_{da}
$$
\n
$$
\tau_{ind} = \begin{cases}\n2 \text{ri} \quad & \text{under the pole faces} \\
0 & \text{begin the pole edges}\n\end{cases}
$$
\n(5.14.1)

(5.14.3)

(5.14.4)

Since
$$
A_p \equiv \pi r / \text{ and } \phi = A_p B
$$

$\tau_{ind} = \begin{cases} \frac{2}{\pi} \phi i & under the pole faces \\ 0 & beyond the pole edges \end{cases}$
The torque in any real machine depends on the following fact that the function is ϕ .
The current in the machine;
The current in the machine;
The constant representing the construction of the machine.

The torque in any real machine depends on the following factors:

- 1. The flux inside the machine;
- 2. The current in the machine;
-