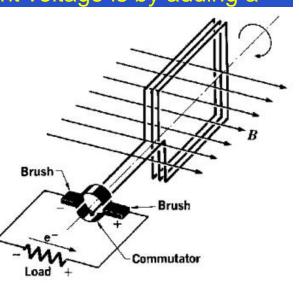
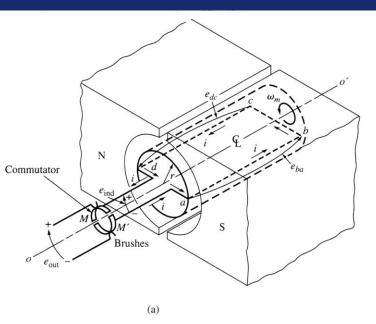
2. Getting DC voltage out of a rotating loop

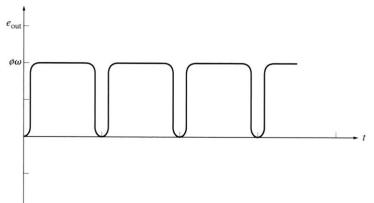
A voltage out of the loop is alternatively a constant positive value and a constant negative value.

One possible way to convert an alternating voltage to a constant voltage is by adding a

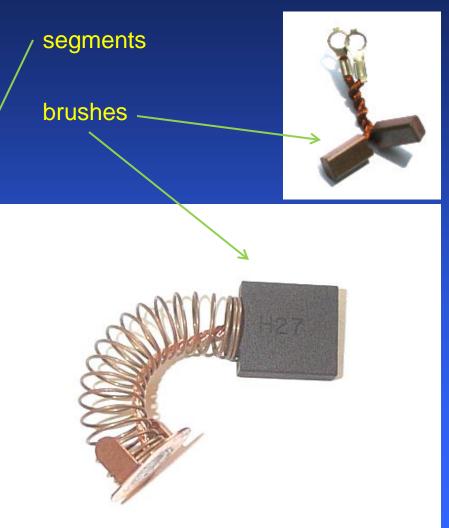
commutator segment/brush circuitry to the end of the loop. Every time the voltage of the loop switches direction, contacts switch connection.

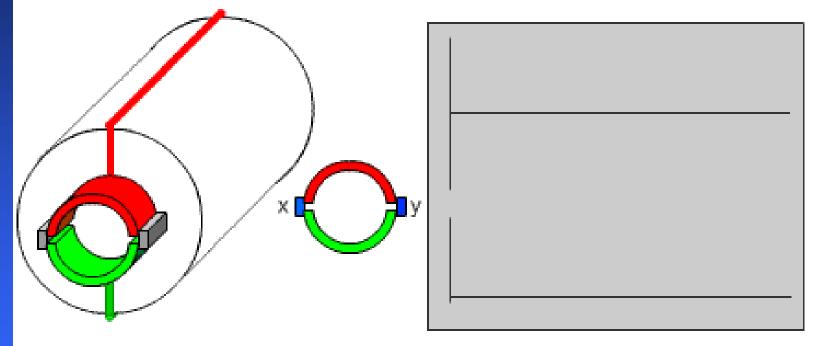












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The tangential velocity of the loop's edges is

$$v = r \omega \tag{5.8.1}$$

where *r* is the radius from the axis of rotation to the edge of the loop. The total induced voltage:

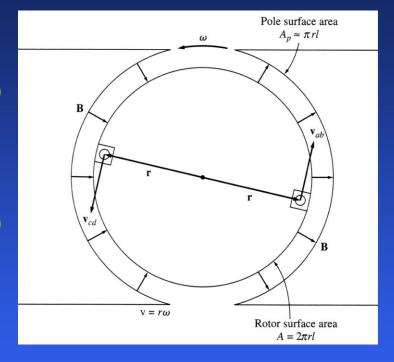
 $e_{tot} = \begin{cases} 2r\omega Bl & under the pole faces \\ 0 & beyond the pole edges \end{cases}$ (5.8.2)

The rotor is a cylinder with surface area $2\pi rl$. Since there are two poles, the area of the rotor under each pole is $A_p = \pi rl$. Therefore:

$$e_{tot} = \begin{cases} \frac{2}{\pi} A_p B \omega \\ 0 \end{cases}$$

under the pole faces

beyond the pole edges



(5.8.3)

Assuming that the flux density *B* is constant everywhere in the air gap under the pole faces, the total flux under each pole is

$$\phi = A_p B \tag{5.9.1}$$

(5.9.2)

The total voltage is

$$e_{tot} = \begin{cases} \frac{2}{\pi} \phi \omega & \text{under the pole faces} \\ 0 & \text{beyond the pole edges} \end{cases}$$

The voltage generated in any real machine depends on the following factors:

- 1. The flux inside the machine;
- 2. The rotation speed of the machine;
- 3. A constant representing the construction of the machine.

3. The induced torque in the rotating loop

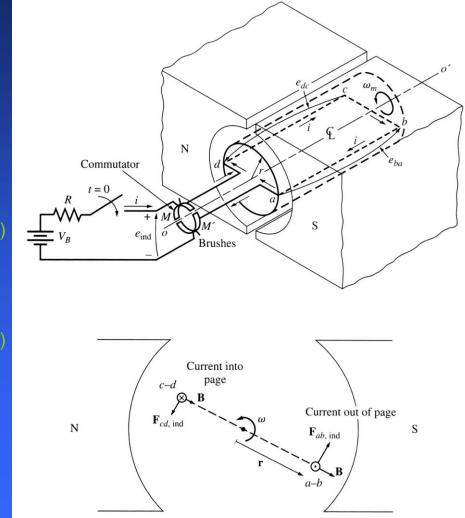
Assuming that a battery is connected to the DC machine, the force on a segment of a loop is:

 $F = i(\mathbf{l} \times \mathbf{B}) \tag{5.12.1}$

And the torque on the segment is

$$\tau = rF\sin\theta \tag{5.12.2}$$

Where θ is the angle between *r* and *F*. Therefore, the torque is zero when the loop is beyond the pole edges.



When the loop is under the pole faces:

1. Segment *ab*: $F_{ab} = i(\mathbf{l} \times \mathbf{B}) = ilB$ (5.13.1)

$$\tau_{ab} = rF\sin\theta = r(ilB)\sin90^\circ = rilB \quad ccw \tag{5.13.2}$$

2. Segment *bc*: $F_{ab} = i(\mathbf{l} \times \mathbf{B}) = 0$ (5.13.3)

$$\tau_{ab} = rF\sin\theta = 0 \tag{5.13.4}$$

3. Segment *cd*: $F_{ab} = i(\mathbf{l} \times \mathbf{B}) = ilB$ (5.13.5)

$$\tau_{ab} = rF\sin\theta = r(ilB)\sin90^\circ = rilB \quad ccw \tag{5.13.6}$$

4. Segment *da*: $F_{ab} = i(\mathbf{I} \times \mathbf{B}) = 0$ (5.13.7)

 $\tau_{ab} = rF\sin\theta = 0 \tag{5.13.8}$

The resulting total induced torque is

$$\tau_{ind} = \tau_{ab} + \tau_{bc} + \tau_{cd} + \tau_{da}$$
(5.14.1)
$$\tau_{ind} = \begin{cases} 2rilB & under \ the \ pole \ faces \\ 0 & beyond \ the \ pole \ edges \end{cases}$$
(5.14.2)

(5 14 3)

Since
$$A_p \cong \pi r l$$
 and $\phi = A_p B$

$$\tau_{ind} = \begin{cases} \frac{2}{\pi} \phi i & \text{under the pole faces} \\ 0 & \text{beyond the pole edges} \end{cases}$$

The torque in any real machine depends on the following factors:

- 1. The flux inside the machine;
- 2. The current in the machine;
- 3. A constant representing the construction of the machine.